A laboratory scale synthesis of geopolymer from demolished-cement-sand-mixture

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ABSTRACT

The demolition of old houses and the construction of new buildings in Kathmandu valley are in the peak in recent days which in turn generates a huge amount of demolished-cement-sand-mixture (DCSM) waste. This DCSM waste is rich source of alumino-silicate and thus used as raw material for the synthesis of geopolymer in this study. Geopolymers have been synthesized from DCSM waste using NaOH and Na₂SiO₃ as activators. Some parameters like alkali concentration, particle size variation, ratio of Na₂SiO₃ to DCSM waste and curing time have been varied in order to improve the quality of geopolymeric product. The results obtained revealed the maximum compressive strength of 46.95 MPa at the ratio of sodium silicate to DCSM waste of 1.5 (w/w) on 28 days curing time at 40 °C temperature.

Keywords: Geopolymer, synthesis, alumino-silicate, waste

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INTRODUCTION

According to the United Nation Statistics Division (UNSD) "wastes are materials that are not prime products (*i.e.* product produced in the market) for which the generator has no further use in terms of his/her own purposes of production, transformation or consumption and of which he/she wants to dispose". Waste may be generated during the extraction and processing of raw materials into intermediate and final products, the consumption of final products and other human activities (United Nations 1997).

In recent years, demolition of old buildings and construction of new ones in most of the major cities is in peak. But due to rapid urbanization and increasing population the empty land spaces are decreasing while land prices are increasing. Several million tons of concrete waste are produced every year due to frequent building demolition and have resulted in drastic reduction in available landfill space due to industrialization and urbanization.

The major composition of the demolished-cement-sand-mixture waste is sand and cement which are the major sources of Al₂O₃ and SiO₂. The prominent application of the aluminosilicate rich materials are the synthesis of light weight aggregates, decontamination of feed contaminated by fungi and mycotoxins, synthesis of zeolites and geopolymer etc.

The term "geopolymer" was coined by Davidovits in 1972 to the tri-dimensional alumino-silicate that are formed at the low temperature and short time by naturally occurring alumino-silicate (Davidovits 1988a). Geopolymer describes a family of mineral binders that have polymeric Si-O-Al

framework structure similar to that found in zeolites because they have approximately same Al: Si ratio.

Geopolymer cement is synthesized from raw material containing alumino-silicate at low temperature which leads to significant reduction in energy consumption and CO₂ emission. It is reported by Davidovits that about 3/5 less energy is required and 80- 90% less CO₂ is generated for the production of geopolymer cement than that of ordinary Portland cement (OPC) (Davidovits 1994). Thus geopolymer cement reduces global warming and saves energy. Furthermore, geopolymer cement possesses high temperature resistance up to 1200 °C without properties degradation. This merit of geopolymer can be applied in automotive and aerospace industries. At present, some geopolymeric products have been used in aircraft to eliminate cabin fire and other aircraft accidents (Comrie 1988).

The primary work on geopolymerization was done on kaolinite and metakaolinite by Davidovits. The mixture of granulated blast furnace slag, kaolinite and metakaolinite showed the highest compressive strength of 79 MPa at 28 days and 60 °C curing time and temperature (Davidovits 1984; Cheng and Chiu 2003). Geopolymer synthesized from metakaolinite at 65 °C curing temperature for 35 days curing time had the compressive strength of 35 MPa (Wang et al. 2005). The adhesive strength of maetakaolinite based geopolymer coating on stainless and mild steel substrate with the composition of Si: Al = 2.5 were found to have the strength >3.5 MPa when cured at 70 °C (Temuujin et al. 2009). The coal combustion fly ashes based geopolymers had gained the compressive strength about 60 MPa when

treated with 12M NaOH and cured at 80 °C for 48 hours (Álvarez-Ayuso et al. 2008). High strength geopolymers with compressive strength over 100 MPa were obtained from coal fly ash, blast furnace slag with potassium silicate solution and water, in which the fly ash was the major the component (Nugteren et al. 2009). The geopolymers with compressive strength in the range of 12.5-56 MPa were synthesized from fly ash (FA) and rice husk ash (RHA) in which sodium silicate to NaOH mass ratio was 4 and curing temperature and time were 60 °C for 48 hours respectively (Detphan and Chindaprasirt 2009). The geopolymers from mechanochemically treated clinoptilolite using NaOH and sodium silicate solutions showed increasing compressive strength up to around 25 MPa with increasing curing time (Jha and Hayashi 2009).

The demolished-cement-sand-mixture waste is the growing problem in many countries and the present study is the preliminary investigation on the possibility of utilizing construction waste as raw materials in the production of geopolymer cement in order to find out the amicable solution for such problem.

EXPERIMENTAL METHODS

Sample preparation

The demolished-cement-sand-mixture (DCSM) waste was selected from demolition area near Nayabazar Kirtipur, Kathmandu and did not include brick and gravel. At first, the pieces of DCSM was ground in iron mortar using pestle with constant sieving until the grain size was reduced to $<100\mu m$. The powder was dried on oven at 60 °C.

Preparation of DCSM base geopolymer

To synthesize geopolymer from cement-concrete waste, several parameters like alkali concentration, powder particle size, amount of sodium silicate and curing time were varied

Variation of NaOH concentration

From 2 to 8N NaOH solutions were prepared separately. About 11gm of DCSM Waste was weighted and was blended manually for 2 minutes with about 4 ml of NaOH solution of various concentration separately using mortar and pestle. This mixture was then transferred to plastic mould (length × breadth × height: 2 cm × 2 cm × 2 cm) and was sealed to prevent water loss. Care was taken to avoid air bubbles. This mould was placed in oven for curing at 40 °C for 6 days

Variation of particle size

The DCSM was grounded and sieved in various size sieves. The DCSM powder of different sizes such as \le 53, \le 75, \le 90, \le 120, μ m was collected. 12 g of different size powder were weighted separately and mixed with 4ml of 6N NaOH solution and then transferred into separate plastic mould. Then samples were cured for 10 days at 40 °C.

Variation of sodium silicate concentration

The variation of mass ratio of sodium silicate to 53 μ m sized DCSM powder were set to 0.5, 1.0, 1.5, 2.0. The mixture was thoroughly mixed with 6N NaOH (3 - 3.5 ml) for 2 minutes and transferred to plastic mould. Then moulds were cured for 21 days at 40 °C.

Variation of curing time

With 1.5 mass ratio of Na₂SiO₃ to DCSM powder (53 µm size), the mixture was mixed in the mortar using 6N NaOH (3.5 ml) manually. The mixture was then transferred to plastic mould and cured for 7-28 days in oven at 40 °C. After curing, the solid sample was removed from plastic mould and polished in various sized sand papers (from 400-800 sizes) to get its smooth surface. The area of the solid smooth sample was measured using vernier calliper and was weighed.

The compressive strength of the prepared geopolymers was measured using SLF Load from machine at central material Testing Laboratory, Institute of Engineering Pulchowk Campus, Tribhuvan University. Each data of the compressive strength presented in this paper is the average of three consecutive measurements. The raw samples and fragment from the crushing tests of few characteristic samples were powdered and examined by X-ray diffraction (Bruker D8 Advance Diffractometer, Germany) available at Central Department of Geology, Tribhuvan University, Kirtipur, Kathmandu.

RESULTS AND DISCUSSION

Characterization of waste powder

The raw DCSM was grounded and sieved. The different sizes portions of the powder were separated. The XRD patterns of DCSM of various particle sizes (\leq 53 - \leq 120 μ m) were obtained and are shown in Fig. 1.

The XRD patterns of the DCSM raw materials of various sizes in Fig. 1 have shown the presence of mainly muscovite,

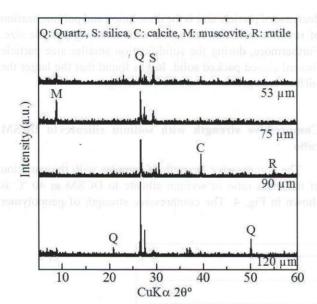


Fig. 1: XRD patterns of raw DCSM of different particle size (53-120 μ m).

quartz, rutile, calcite and silica. The quartz peak $(2\theta=26.69^{\circ})$ was diminished with decreasing the size of particle. Several another peaks were diminished with decreasing particle size while a new peak at $2\theta=27.68^{\circ}$ was appeared which was characterized as SiO_2 . This was expected to be due to the conversion of quartz to silica during the process of mechanical grinding.

It has been reported that mechanical milling can enhance the transformation of crystalline to amorphous phase (ElEskandarany et al. 1997). The diminishing of several XRD peaks and increase of the amorphous nature of the sample with reducing particle size attributed to the fact that the mechanical grinding increases the collision frequency which in turn leads to faster diffusion process (Lü and Lai 1998).

Compressive strength with NaOH concentration variation

Fig. 2 represents the compressive strength of samples with the variation of NaOH concentration. The compressive strength initially increased and then decreased showing the maximum strength of 2.943 MPa at 6N NaOH.

The above results can be interpreted as follows. The dissolution of alumino-silicate take place under alkaline solution and the higher amount of hydroxyl ion facilitate the dissolution of different silicate and aluminate species promoting polymerization (Davidovits 1988b; Yip et al. 2005). But under high alkaline condition the connectivity of silicon anion may be reduced which causes alumina-silicate gel to precipitate at early stage resulting in poor polymerization i.e. NaOH molecule is incorporated between two geopolymer precursors which break the silicon anion connectivity thus preventing polymerisation (Singh et al. 2005).

Further, the excess NaOH forms Na₂CO₃ by atmospheric carbon (Barbosa et al. 1999). Due to these reasons, the excess concentration of NaOH causes the decrease in compressive strength. Having small size, Na⁺ can form strong pair with

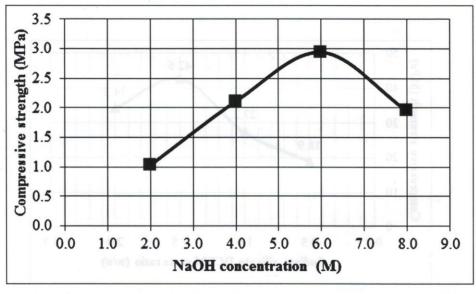


Fig. 2: Plot of compressive strength as a function of NaOH concentration where curing time and temperature were kept constant.

Dipak Paudel et al.

small silicate oligomers and thus stabilize silicate monomer and dimmer; enhancing mineral dissolution (Komnitsas and Zaharaki 2007).

Compressive strength with particle size variation

Fig. 3 represents the compressive strength of geopolymeric products with variation of size of DCSM. Here the compressive strength was found decreasing with increase of particle size.

The reason behind the increase of compressive strength with

decrease of particle size is the dissolution and polymerization of raw material was enhanced with reducing particle size. Furthermore, during the solidification smaller size particle formed closed packed solid. It was found that the larger the surface area greater would be the strength.

Compressive strength with sodium silicate to DCSM ratio

The compressive strength of samples with the variation of the mass ratio of sodium silicate to DCSM at 40 °C is shown in Fig. 4. The compressive strength of geopolymer

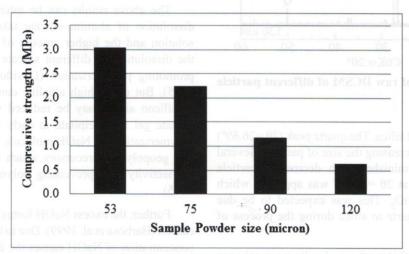


Fig. 3: Plot of compressive strength as a function of particle size variation of DCSM where NaOH concentration, curing time and temperature were kept constant.

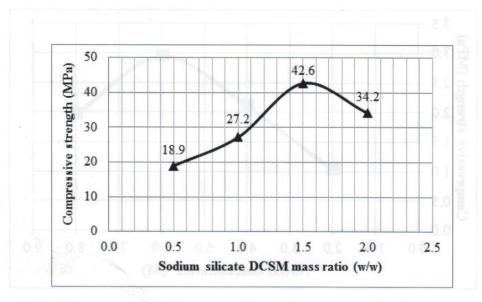


Fig. 4: Plot of compressive strength as a function of mass ratio of Na₂SiO₃ to DCSM where particle size, NaOH concentration, curing time and temperature were kept constant.

was first found to increase and decreased with maximum compressive strength of 42.63 MPa.

It can be well observed from Fig. 2 that after the addition of Na₂SiO₃ the compressive strength increases. This is because at higher concentration of silicates, the stronger ion pair formation is expected which results in formation of longer chain silicate oligomer as well as Al–O–Si complexes (McCormick et al. 1989). Thus added silica acts as a binder shown in the reaction below. But the increased silica decreases the rate of geopolymerization (Provis and van Deventer 2007a) and also in high silica system; solidification of the paste prior to reaction completion may occur (Provis and van Deventer 2007b). This may be the probable reason why increase in amount of silicate causesdecreases in compressive strength.

Further, it is believed that the amount of unreacted materials in the specimen with higher silica content act as the defect site and has the negative effect on strength (Davidovits 1984).

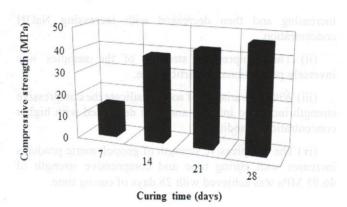


Fig. 5: Change in compressive strength with the variation of curing time where particle size, NaOH concentration, sodium silicate to DCSM mass ratio and curing temperature were kept constant.

$$\begin{array}{c} n(\text{Si}_2\text{O}_5\text{Al}_2\text{O}_2) + 2n\text{SiO}_2 + 4n\text{H}_2\text{O} \xrightarrow{\text{NaOH KOH}} n(\text{OH})_3 - \text{Si}_2 - \text{O}_2 - \text{Al}_2 - \text{O}_2 - \text{Si}_2 - (\text{OH})_3 & \cdots (1) \\ \text{OH} & \text{I} & \text{I} \\ n(\text{OH})_3 - \text{Si}_2 - \text{O}_2 - \text{Al}_2 - \text{O}_2 - \text{Si}_2 - (\text{OH})_3 \xrightarrow{\text{NaOH KCH}} (\text{Na}^+/\text{K}^+) - (\text{Si}_2 - \text{O}_2 - \text{Al}_2 - \text{O}_2 - \text{Si}_2 - \text{O}_2) + 4n\text{H}_2\text{O}_2 - (2) \\ \text{I} & \text{OH} & \text{O} & \text{O}_2 - \text{O}_2$$

In the above formula (1) (SiO₅Al₂O₂) is an emphasized form to stand out the IV fold co-ordination of Al instead of conventional alumino-silicate oxides form of (2SiO₂. Al₂O₃)·SiO₂ in formula (1) is a monomer or polymer form which comes from silicate added later. Formula (2) shows the final backbone of the geopolymer and charge balance in the matrix.

Compressive strength with curing time variation

The compressive strength of geopolymeric products with the variation of curing time at 40 °C is shown in Fig. 5. The compressive strength increases with increase in the curing time with the maximum compressive strength of 46.95 MPa. The strength continues to rise further as shown in the graph above.

Unlike cement, which has fixed life span about 50 years and after which compressive strength decreases, the strength of geopolymer tends to rise. Egyptian pyramid can be taken as the example. This is because once the stable 3D structure of geopolymer is formed it can stay intact for centuries until and unless crack develop due to several reasons like

earthquake and also the resistivity against fire, chemical and high temperature (1200 °C) add the quality of geopolymer but these parameters deteriorates the cement rapidly.

The curing for longer period of time at low temperature is preferable for the synthesis of geopolymer as at low temperature condensation of geopolymer precursors and evaporation of the water molecules takes place simultaneously preventing the formation of voids and cracks inside the material thus increasing the compressive strength.

CONCLUSIONS

The geopolymer was synthesized by using various concentration of alkali activator *i.e.* NaOH and Na₂SiO₃. The parameter like size variation, amount of sodium silicate and curing time were studied at 40 °C curing temperature. The following conclusions were drawn from the experimental results of the study:

(i) The compressive strength was found initially

increasing and then decreased with increasing NaOH concentration.

- (ii) The compressive strength of the samples was inversely proportional to particle size.
- (iii) With the variation of sodium silicate the compressive strength increased initially and then decreased with higher concentration of sodium.
- (iv) The compressive strength of geopolymeric products increases with curing time and compressive strength of 46.95 MPa was achieved with 28 days of curing time.

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